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SHADZO: A COMPUTER PROGRAM FOR ESTI-MATING THE POSITION AND SHAPE OF THE SURFACE SHADOW ZONE IN SONAR OPERATIONS

Bernard de Raigniac, et al

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15 November 1972

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SHADZO: A COMPUTER PROGRAM FOR ESTIMATING THE POSITION AND SHAPE OF THE SURFACE SHADOW ZONE IN SONAR OPERATIONS

by

BERNARD DE RAIGNIAC and JOHN PADLEY



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NORTH ATLANTIC TREATY ORGANIZATION SACLANT ASW RESEARCH CENTRE Viale San Bartolomeo 400 I 19026 - La Spezia, Italy

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Director

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ABSTRACT

SHADZO is a composite program which calculates the position and shape of the first surface shadow zone as a function of the source depth for a given sound speed profile. The program is small enough to be run on a shipboard mini-computer in a few minutes.

INTRODUCTION

It has been found from SACLANTCEN's reverberation studies that information on the position and extent of the surface shadow zone is needed during at-sea experiments. Thus, a program has been developed which, given the sound speed profile, calculates the pertinent characteristics of the shadow zone and can be run on a shipboard mini-computer in a few minutes. In order to make the maximum possible information available to the scientists aboard ship, the program also includes the estimation of shadow zone shape.

SHADZO (surface SHADow Zone program) is a composite program which calculates the position and shape of the surface shadow zone, as a function of the source depth, for a given sound speed profile. These characteristics are obtained by direct investigation of the limiting rays, rather than by representation of the sound field by ray-tracing with a high density of rays.

This memorandum describes the theoretical basis for, and the implementation of, the two basic parts of SHAZDO: (1) a part that calculates the distance (i.e., the inner range limit), the extent and the maximum thickness as functions of source depth, and (2) a part that estimates the shape of the shadow zone for selected source depths. A flow chart, a listing, and explanatory diagrams of SHAZDO are given in Appendix A.

^{*} The surface shadow zone treated here is the first (i.e., shortest-range shadow zone; the recurring surface shadow zones at longer ranges are not covered.

1. THEORY: POSITION AND SHAPE OF THE SURFACE SHADOW ZONE

1.1 Background

When the sound source is located above the critical depth, z_{crit}, there is a shadow zone along the surface at certain ranges. This surface shadow zone has been discussed by Mellberg, who calls it "shadow layer", in Ref. 1. Mellberg provides formulae for the maximum thickness and horizontal extent of the shadow zone, based on a 2-layer, constant gradient model of the medium. The present memorandum provides a further description of the characteristics of the shadow zone, based on a multi-layer, constant-gradient model.

Figures 1 and 2 illustrate the formation of the surface shadow zone in a medium approximated by a two-layer, constant-gradient model. Figure 1a shows the rays which limit the shadow zone, both in range and depth, when the source is between the surface and the minimum-speed-depth, z_m . At the surface, the shadow zone is bounded by rays which have zero grazing angle. The maximum depth, or maximum thickness of the shadow zone, is the depth at which the ray that was horizontal at the source becomes horizontal again. When the source is located between the minimum-speed depth z_m and the critical depth, z_{crit} , as in Fig. 1b, a shadow zone of smaller range extent and smaller maximum thickness will occur.

Figure 2 illustrates the distance, extent and maximum thickness of the shadow zone, again for a 2-layer model. The multi-layer model will be introduced next, and then these three characteristics will be discussed in turn.

The critical depth is the depth at which the sound speed is the same as at the sea surface

In SHADZO, a multi-layer, constant-gradient model of the medium is used. The rays propagate along circle segments in each layer, as illustrated in Fig. 3. The radius of the path in the ith layer is given by:

$$R_1 = \frac{k}{g_i}$$
 [Eq. 1]

where

Herefield hands and the state of the state o

k = Snell's constant of the ray
= c/cos@ (at any depth)

 $g_i = \text{gradient in the ith layer}$ $= \frac{c_i - c_{i-1}}{\Delta z_i}.$

The horizontal distance travelled by the ray in the ith layer is then:

$$\Delta d_{i} = R_{i} (\sin \alpha_{i-1} - \sin \alpha_{i})$$

$$= \Delta z_{i} \frac{\sqrt{k^{2} - c_{i-1}^{2}} - \sqrt{k^{2} - c_{i}^{2}}}{c_{i} - c_{i-1}}.$$
 [Eq. 2]

1.2 Distance

The distance to the shadow zone. 's illustrated in Fig. 2, is defined as the inner range limit of the shadow zone at the surface.

Appendix A of Ref. 2 provides formulae for the distance, for both 2-layer and multi-layer constant-gradient models.

From Eq. 2, we see that the total horizontal distance, d, travelled by a ray in traversing n layers between the source depth and the surface is given by

$$d = \sum_{i=1}^{n} \Delta d_{i} = \sum_{i=1}^{n} \Delta z_{i} \frac{\sqrt{k^{2} - c_{i-1}^{2}} - \sqrt{k^{2} - c_{i}^{2}}}{c_{i} - c_{i-1}}.$$

To avoid computing errors when $c_i \approx c_{i-1}$, this expression may be transformed into

$$d = \sum_{i=1}^{n} \Delta z_{i} \frac{c_{i-1} + c_{i}}{\sqrt{k^{2} - c_{i-1}^{2}} + \sqrt{k^{2} - c_{i}^{2}}}.$$
 [Eq. 3]

d may be expressed as a function of grazing angle at the surface, γ , by writing $k=c_0/\cos\gamma$. Thus, we see that the distance to the shadow zone, D, is obtained from Eq. 3 simply by setting $\gamma=0$; then, we have $k=c_0$ and

$$D = \sum_{i=1}^{n} \Delta z_{i} \frac{c_{i-1} + c_{i}}{\sqrt{c_{o}^{2} - c_{i-1}^{2}} + \sqrt{c_{o}^{2} - c_{i}^{2}}}.$$
 [Eq. 4]

1.3 Extent

The horizontal extent of the shadow zone at the surface is determined by two rays having zero grazing angle, as illustrated in Fig. 2. It can be seen from Fig. 2 that the horizontal distance travelled by the long-range limiting ray in going between source depth and critical depth is a measure of the extent of the shadow zone. Thus, the extent is given by

$$E = 2 \sum_{i=n+1}^{k} \Delta z_{i} \frac{c_{i-1} + c_{i}}{\sqrt{c_{0}^{2} - c_{i-1}^{2}} + \sqrt{c_{0}^{2} - c_{i}^{2}}}$$
[Eq. 5]

where it is assumed that there are n layers between the source depth and the surface and k layers between the critical depth and the surface.

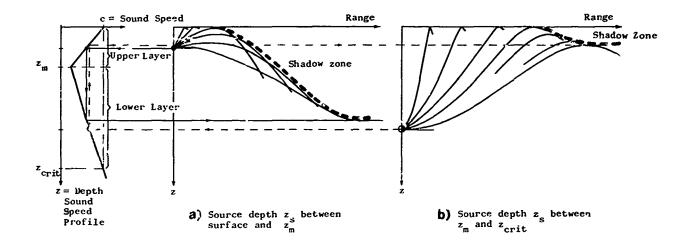
1.4 Maximum Thickness

As discussed in Ref. 1 and illustrated in Figs. 1 and 2, the maximum depth of the shadow zone is the depth where a ray that was horizontal at the source becomes horizontal again. At this depth, z_t , the sound speed is equal to c_s , the sound speed at source depth.

1.5 Shape

The shape of the shadow zone can be defined as the envelope of the downward-refracted rays, as illustrated by the dashed curves in Fig. 1. This envelope is relatively difficult to calculate exactly, so an estimate of the shape is obtained as follows. First, at close-y-spaced depths, we determine the logus of points at which rays vertex (i.e. become horizontal). For the case shown in Fig. 1b, we see that this locus would provide a reasonable estimate of the envelope*. Figure 4 illustrates the case of a limiting ray, such as might be encountered in the presence of a strong negative gradient; in this case, the locus of vertices is not a good estimate. To improve the estimate, at each depth, the intersections of rays vertexing at shallower depths are determined. Finally, at each depth, that point (vertex or intersection) is used which results in the smallest extent of the shadow zone. The estimation of shat w zone shape from these vertices and intersections is illustrated in Fig. 4.

It would be clearly not provide a reasonable estimate for the case in Fig. 1a; nowever, this case is not addressed here, as the snape estimation part of SHADZO has been implemented only for cases in which z>z, z=z



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FIG. 1 FORMATION OF THE SHADOW ZONE

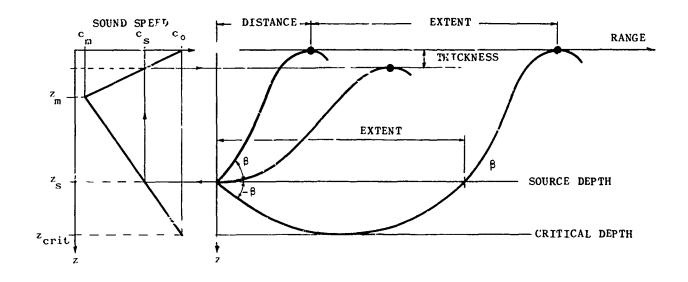


FIG. 2 DISTANCE, EXTEN (AND MAXIMUM THICKNESS OF THE SHADOW ZONE

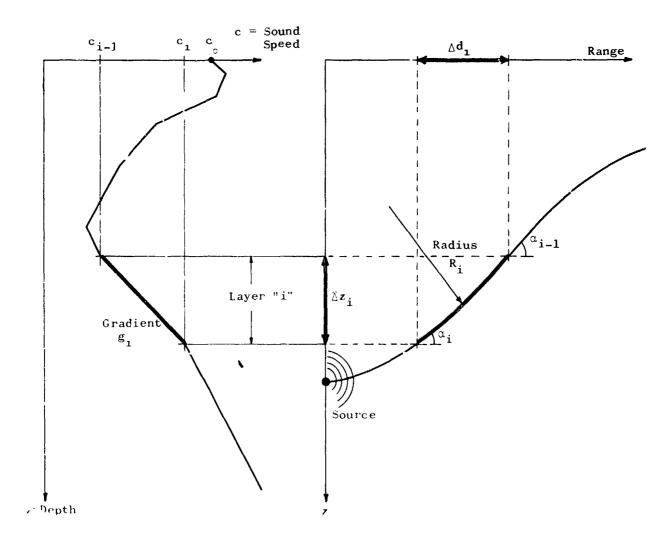


FIG. 3 KAY PATH IN A MULTI-LAYER, CONSTANT-GRADIENT MEDIUM

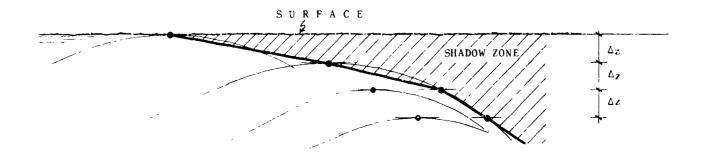


FIG. 4 ESTIMATION OF SHADOW ZONE SHAPE

2. DESCRIPTION OF THE SHADZO PROGRAM

2.1 Hardware Configuration

The program was written to run under the Hewlett-Packard Real-Time System [Ref. 3], and thus requires a minimum hardware configuration of:

H-P 2116B Computer with 16K Memory

H-P 12578A Direct Memory Access

H-P 12579A Extended Arithmetic Unit

H-P 12591A Memory Protect

Fixed Head Disc or Drum Storage Unit

Time Base Generator

Operator Console (ASR-33 or ASR-35 Teleprinter)

In addition, the SHADZO program requires a Tektronix T4002/4802 Graphic Computer Terminal with Tektronix Joystick 015-0175000 and Hard Copy Unit 4601. The Tektronix Terminal can be used in place of the operator console, if an additional paper-tape input device is available. In the absence of a Tektronix Terminal, the program can still produce a printed output on any output writer.

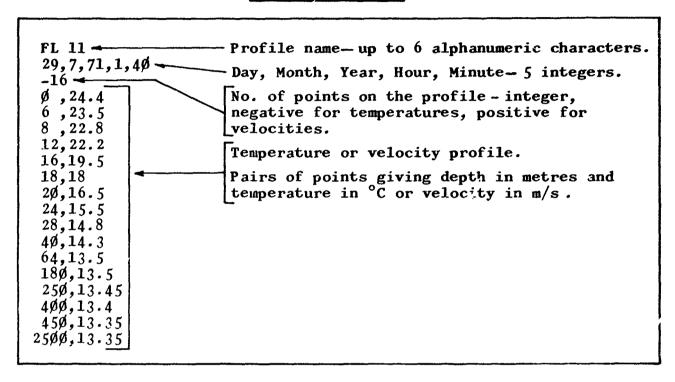
2.2 <u>Sottware Configuration</u>

The program requires a Real-Time System generated to provide a minimum background disc-resident area of 20K (octal) locations. The Tektronix Terminal should be allocated logical unit number 16 and should be used with the Real-Time teleprinter driver DRVOO.

2.3 Program Inputs

The data are input to the program via a punched tape containing the temperature or sound speed profile. Table 1 gives an example of such a profile, as well as the required format.

TABLE 1
TYPICAL DATA TAPE



In the conversion from temperature profile to sound speed profile [according to the Leroy formula (Ref. 4)], the salinity and longitude are considered constants, being pre-set to 38.6 parts/thousand and 40° , respectively. Source depth values are input via the Operator Console.

2.4 Program Details

The SHADZO² program is written in Fortran II, with the exception of the routines for the Tektronix Terminal, which are standard SACLANTCEN library routines written in Assembler Code.

The program consists of four basic sections, as follows:

Section One Reading of the data tape tape, and conversion

of temperatures to sound speeds it necessary.

Section Two: Calculation and printing of distance, extent

and maximum thickness.

Section Three: Calculation and graphical display of distance,

extent and maximum thickness.

Section Four: Calculation and graphical display of shadow

zone shape.

The first section is performed once for each set of data; the other sections are performed as many times as required.

Sections two and three can be run with two alternative models of the sound speed profile: (1) a multi-layer, constant-gradient model, using all of the sound speeds calculated from the Leroy formula; and (2) an approximation using two constant-gradient layers.

Because of the restriction in H-P Fortran II which allows only five characters per identifier, the program name actually used is "SHAZO". There are some discrepancies between the terminology used in the text of this memorandum and the terminology used in the program and its outputs shown below. The correspondence is as follows:

lerm in lext	Term in Program
Sound speed	Velocity
Maximum thickness	Thickness
Distance	Range
Extent	Extension

A flow chart and listing of the program, together with diagrams indicating the significance of variable names for points on the sound speed profile, are given in the appendix.

2.5 Program Outputs

The outputs from the program are prints and plots, as described below.

2.5.1 Prints

a. Sound speed profile: A sample output is given in .Table 24

TABLE 2

EXAMPLE OF SOUND SPEED PROFILE GUTPUT

SHADOW ZONE PREDICTIONS

XBT FL 11	DATE 29-7-	-71 TIME 1-48
DEPTHS	VELOCITIES	
METRES	METRES/SEC	
.øø	1537.3	
6.ØØ	1535.2	
8.00	1533.5	
12.ØØ	1532.1	
16.ØØ	1525.Ø	
18.ØØ	152Ø.8	
2Ø.ØØ	1516.4	
24.00	1513.5	
28.øø	1511.4	
40.00	151ø.ø	
64.ØØ	15Ø7.8	
18ø.øø	1509.7	
25Ø.ØØ	151Ø.7	
400.00	1513.Ø	
450.00	1513.7	
25øø.øø	1548.ø	

b. Distance, extent and maximum thickness: An example is given in Table 3 for the multi-layer model. The output from the two-layer model has a similar format.

TABLE 3

EXAMPLE OF SHADOW ZONE CHARACTERISTICS GUTPUT

MULTILAYER MODEL

SOURCE DEPTH	EXTENSION	RANGE	THICKNESS	S. VELOCITY
METRES	METRES	METRES	METRES	M/SEC
1 55. 5	35826.4	794-3	57.5	15\$8.4\$
26€.€	34794.9	1316.6	39.8	1510.00
3 56. 6	33733.8	1846.6	27.8	1511.48
499.9	32648.1	2387.4	24.9	1513. \$ 2
5 66. 6	31511.9	2951.6	22.6	1514.52
6 55. 5	3\$341.5	3536.8	26.3	1516.26
7 95. \$	29122.7	4146.2	19.3	1517.87
8 \$\$.\$	27849.2	4782.9	18.6	1519.55
9 øø .ø	26513.1	5451.Ø	17.8	1521.22
1 989. 8	251\$4.4	6155.3	17.ø	1522.9ø
11 \$\$. \$	2361ø.1	69 \$2. 5	16.2	1524.57
12 \$\$.\$	22012.7	77Ø1.2	15.3	1526.25
13 \$\$.\$	2 \$ 288.i	8563.5	14.4	1527.92
14ØØ.Ø	184øø.3	95\$7.4	13.4	1529.59
15ØØ.Ø	16292.9	1ø561.1	12.5	1531.27
16 øø.ø	13865.9	11774.6	9.6	1532.94
17ØØ.Ø	10908.2	13253.4	6.7	1534.62
18ØØ.Ø	6755.3	15329.9	3.Ø	1536.29

2.5.2 Plots

All graphical outputs are plotted on the Tektronix Terminal and have a similar format. The results are plotted on a 5 x 5 grid and a scale factor for each parameter is printed on the display; this scale factor is the number of metres equivalent to one division of the display (i.e., full scale is five times the scale factor). At the end of each display, a copy is produced on the Hard Copy Unit. The origin of the plot is the upper left hand corner; the vertical

parameter is depth and the other relevant parameter is plotted horizontally.

- a. Distance, extent and maximum thickness: one plot is produced for each parameter. Examples are given in Fig. 5.
- b. Shape: One plot is produced. If more than one source depth is requested, all outputs are plotted on the same graph to the same scale. An example is given in Fig. 6.

2.6 Operation

To run the program, load the data tape in the tape reader and enter the program (under the Real-Time System, this is effected by typing "ON, SHADZO" on the Operator Console). If the last point on the temperature or sound speed profile is not deep enough to allow the critical depth to be calculated, the computer prints:

THE LAST POINT OF THE B.T. IS ABOVE THE CRITICAL DEPTH

and the program ends. In this case, the data tape must be retyped. Once a correct data tape has been read and the sound speed profile has been calculated and listed as shown in Table 2, the computer will print:

FOR SHADOW ZONE SHAPE TYPE 1 OTHERWISE TYPE -1 *

- 2.6.1 Distance, Extent and Maximum Thickness:
- If -1 is replied to the question about shadow zone shape, the computer outputs:

FOR GRAPHIC OUTPUT TYPE 1 OTHERWISE TYPE -1

All questions of this type should be answered by either -1 or 1, followed by carriage return, line feed.

and after the response to this request, the computer outputs:

AND THE PERSON OF THE PERSON O

FOR MULTILAYER TYPE 1, FOR 2 LAYER TYPE -1

When the type of model has been selected, if no graphic output was requested, then the computer prints:

TYPE IN S. DEPTH: START, STEP, END

The source depths for which output is required should then be typed in, giving the minimum depth first, and with values separated with commas. No output is produced for source depths greater than the critical depth. When the source depth has been input, the results are calculated and printed.

If graphic output is selected, then the three graphs are displayed and after the last output, the joystick is enabled and the computer prints:

TO EXPAND PLOT POSITION CURSOR AT MAXIMUM SOURCE DEPTH REQUIRED AND TYPE 1 OTHERWISE TYPE \emptyset

If an expansion is required, then the horizontal line of the cursor should be placed at the maximum source depth for the new plots and 1 should be typed. A new set of lisplays is then produced, and the expansion option is repeated. (It is not possible at this stage to increase the maximum source depth of the display. If this is required, the program must be continued and reprocessing of the same data requested. See below). If expansion of the plots is not required, type 0.

2.6.2 Shadow Zone Shape

THE THE PARTY OF T

If the shape is requested, then the source depths are requested as for the printer output above. The source depths must be below the depth of minimum sound speed; if the starting depth is less than this value, then it is automatically adjusted to this value.

If the source depth exceeds the critical depth, the calculation stops. If only one source depth is required, the second and third parameters should be zero. The computer then calculates and displays the shape.

2.6.3 Termination

After the relevant output has finished, the computer prints:

TYPE \$ TO REPROCESS, 1 TO PROCEUR NEW DATA OK 2 TO STOP

If the response is 0, the program returns to the point at which it asks if the shadow zone shape is required. If the response is 1, a new data tape is read and processing restarts. If the response is 2, the program ends.

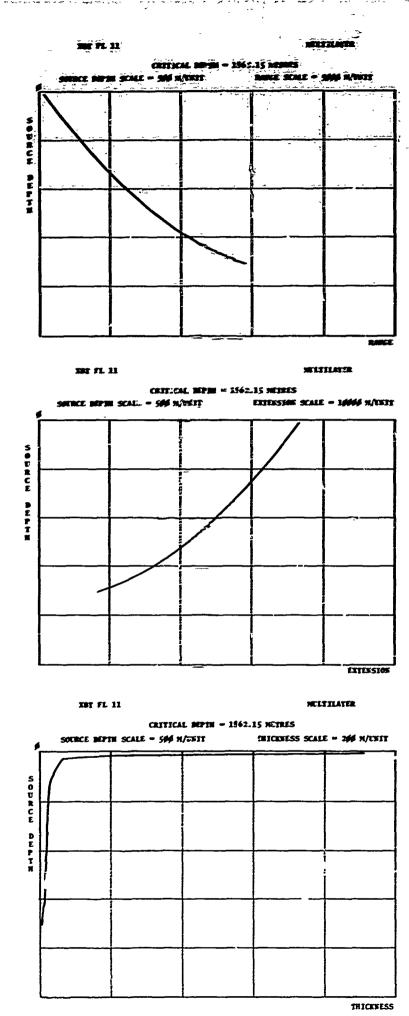
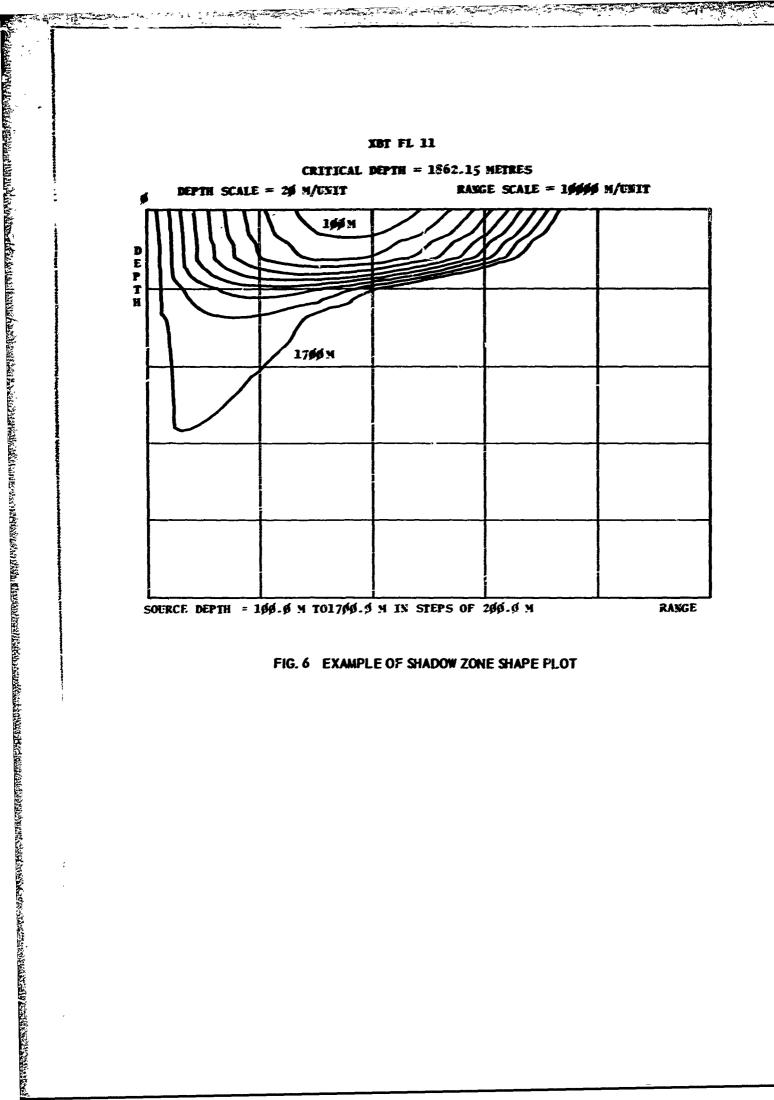


FIG. 5 EXAMPLES OF DISTANCE (RANGE), EXTENT (EXTENSION) AND MAXIMUM THICKNESS PLOTS



REFERENCES

- Mellberg, L.E., "Optimum Sonar Transducer Depths for Decreasing the Effects of Surface Reverberation (NU)", SACLANTCEN Technical Report No. 167, April 1970, NATO CONFIDENTIAL: [AD No. 510 235]
- Bachmann, W. and de Raigniac, B., "The Calculation of the Surface Backscattering Coefficient of Underwater Sound from Measured Data", SACLANTCEN Technical Memorandum No. 174, November 1971, NATO UNCLASSIFIED.

[AD No. 735 995]

- 3. "Real Time Software, A Reference Text for Programmers", Hewlett-Packard Co. Document No. HP 02005-90002, October 1971.
- 4. Leroy, C.C., "Development of Simple Equations for Accurate and More Realistic Calculation of the Speed of Sound in Sea Water", SACLANTCEN Technical Report No. 128, November 1968, NATO UNCLASSIFIED. [AD No. 845 866]

APPENDIX A

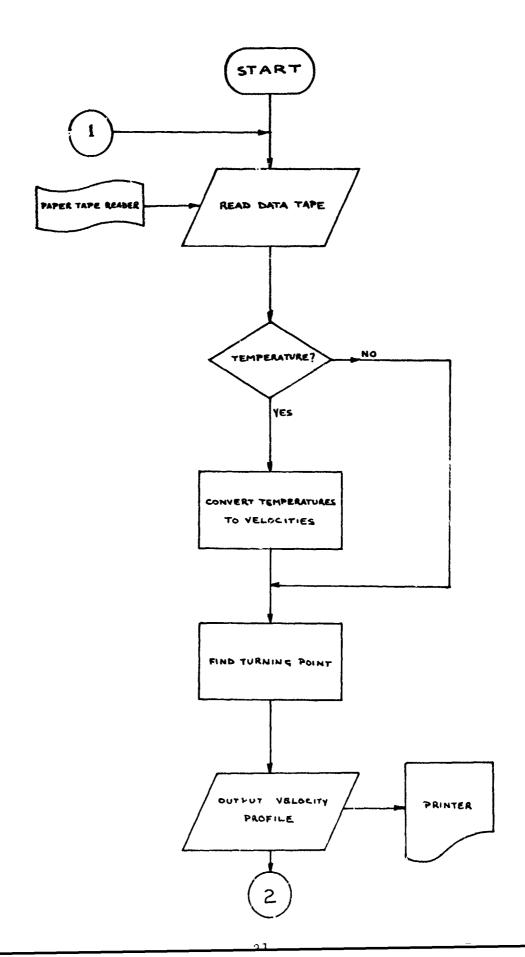
DETAILED PROGRAM INFORMATION

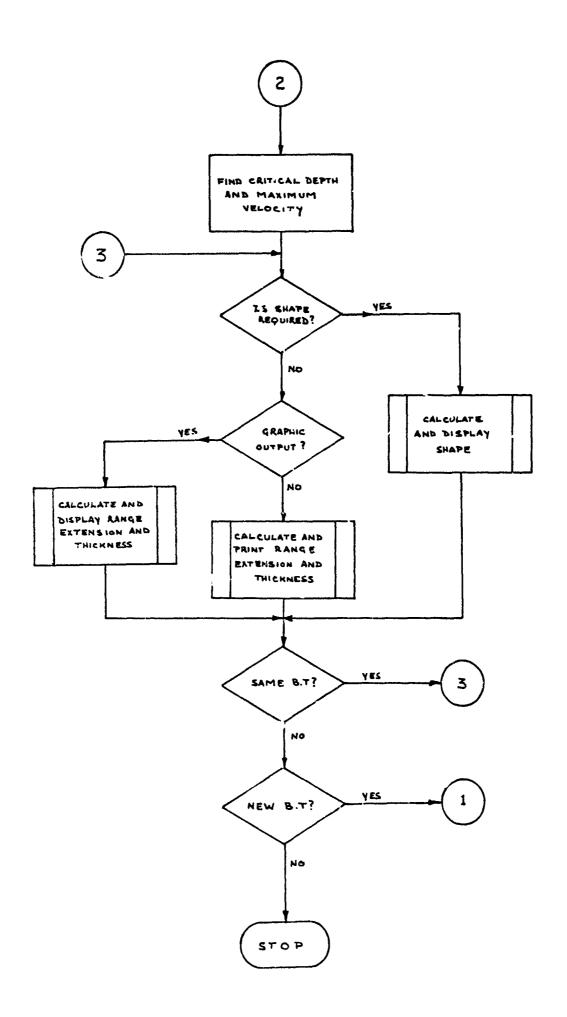
- A.1 Flow Chart
- A.2 Explanatory Diagrams and Program Listing

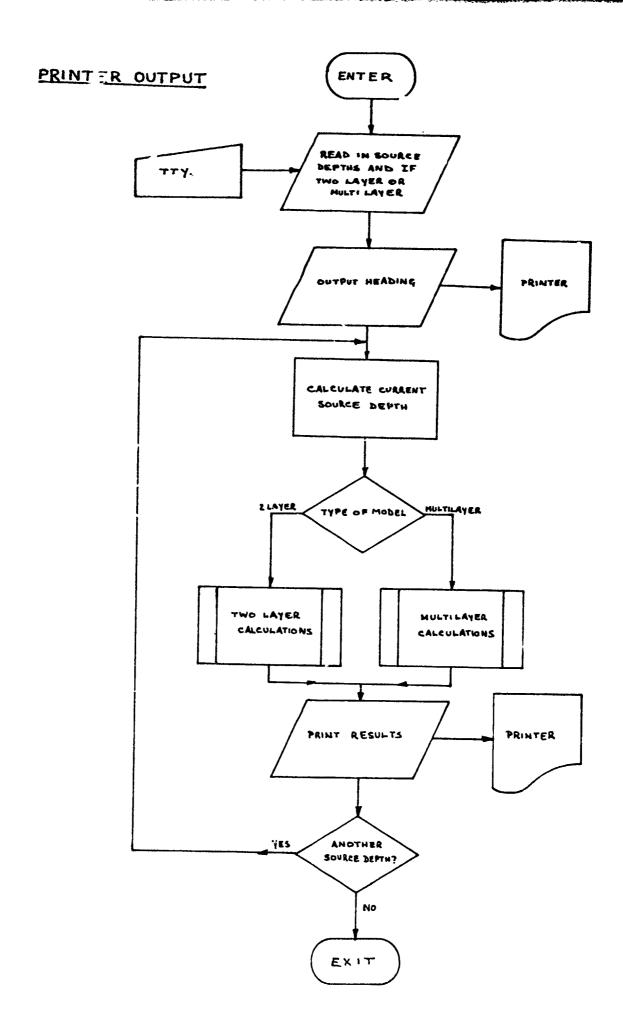
Note: The word "velocity" used in this Appendix corresponds to the words "sound speed" used in the Main Text.

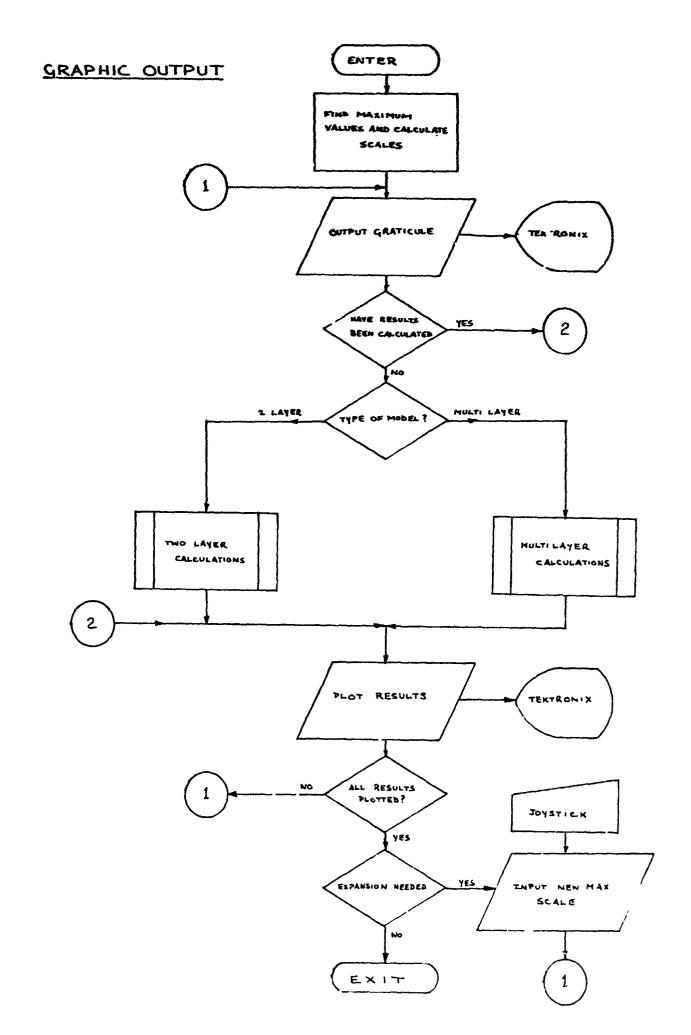
A.1 Flow Chart

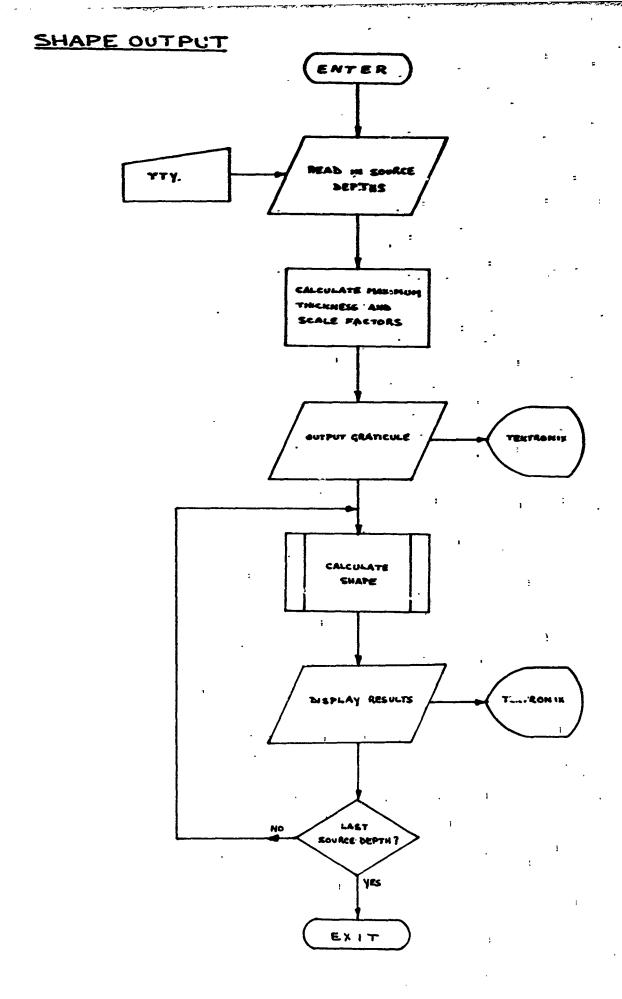
SHADZO FLOW CHART



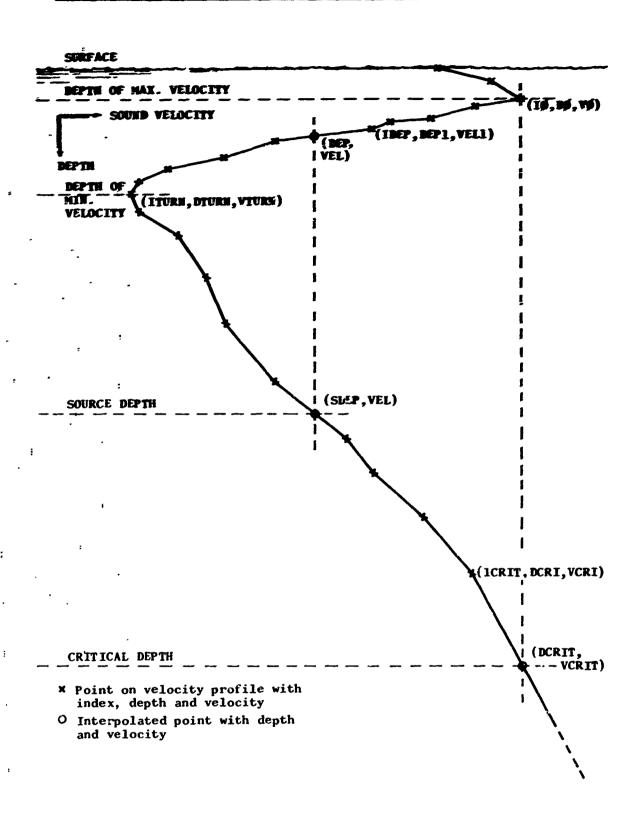




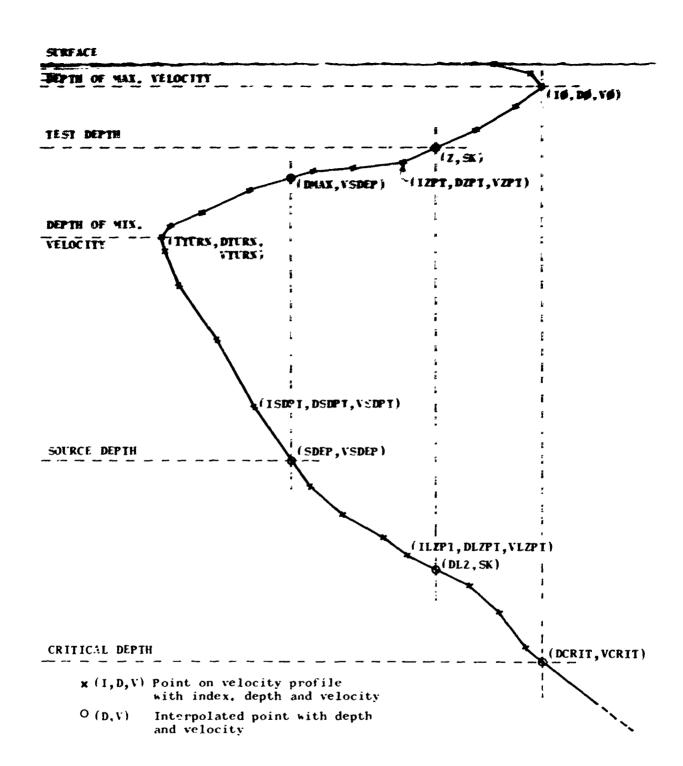




A.2 Explanatory Diagrams and Program Listing



PARAMETERS USED IN CALCULATION OF RANGE, EXTENSION AND THICKNESS



PARAMETERS USED IN CALCULATION OF SHAPE

```
FTM.L
C
           THIS PEUGLAM HAS BEYELDPED AT -
C
C
                     SACLANT ASS RESEARCH CENTRE
C
                     VIALE SAM BARTOLOMED. 489
C
                      14026, LA SPEZIA
C
                     ITALY.
C
      PROSERT Smale (3,76)
C
           J.F. 27-14-71
·C
      DIMENSION ((40), V(+4), C(+6), IASCI(18), INAME(6)
      DIMERSION PA(150) .EX(120)
C
           THIS PROGRAM PREDICTS THE RANGE AND EXTENSION
C
C
      OF THE SHADOW ZONE FOR VARIOUS SOURCE DEPTHS.
C
C
           READ DATA TAPE AND CUNVERT TEMPERATURES TO
C
      VELOCITIES IF MECESSARY.
C
      PHI=42.
      SAL=38.6
   10 DO 23 I=1.6
   20 INAME(1)=200433
      READ (5,3%) (INAME (1), I=1,6)
   30 FORMAT (BAI)
      TUNIMARUCHI AKABYI ANTHONIA YACI (*.5) CABR
      READ(5.2) MODE
      N=I485 (XUSE)
      DO 35 I=1.N
   35 READ(5.*) 0(I) .v(I)
       IF (MODE) 48+5#
   48 CALL BIRAN(V.D.N.SAL,PHI)
   50 CALL FINT? (V.N. ITURN)
      DTURN=C(ITURN)
      VTuRN=V(ITURN)
           OUTPUT HEADING AND VELOCITY PROFILE
      CALL EXEC (3,11668,-1)
      TIPE (1) ATEC (6,62) (INAME (1) • I=1 • (1) ATEC (6,62) (6,62)
   60 FORMAT(24%. MSHADOW ZONE PREDICTIONS", //, 7%, WABT ", 6A1,
           12**"J45E"+13*2("-"*12)*12X*"TIME"*13*"-"*12*//*
           5x . "DEPTHS" . 10x . "VELOCITIES"/5X . "METRES" . 10X .
     2
           "METRES/SEC"+/)
       WRITE(6,7%)(D(I),√(I),1=1,N)
   70 FORMAT (X) F16.2, F17.1)
           FIND CHITICAL DEPTH ETC.
       IF (v(v)-Vv) 30,100
   88 WRITE(1.90)
   90 FORMAT ("THE LAST POINT OF THE B.T. IS ABOVE THE ",
           "CFITICAL DEPTH")
```

```
PAGE " 7022
      STSP
  1-2 52=5(1)
      りまニ た。
      IZ=1
      CO 12# I=2-1703%
      IF (# == (I)) 1196129:
  112 42=2617
      D==3(1)
      I==1
  120 CONTINUE
      CALL FIRML (17-10-122-UCFIT-ICRIT-M-ITURN)
      VCHIT=VZ
      WRITE (E. 139) DCRIT
  134 F@R#AT(/512X54CRITICAL DEPTH =M5F8.2. M METRESM/)
C
C
          REGUEST TYPE OF CALCULATION AND OUTPUT
C
  146 $PITE(1:145)
  145 F F 147, MEDIE STADON ZONE SHAPE TYPE 1 OTHERWISE TYPE -1 +*)
      RESD(1:#) ISHAP
      IF (15452) 154,720
  15# #-17E(1-165)
  155 FG-84T("Fux beaPaiC OUTPUT TYPE 1 OTHERWISE TYPE -1 +")
      READ (1.4) IGRAP
      MEITE (inlaw)
  169 FORMAT ("FOR MULTILAYER TYPE 1, FOR 2 LAYER TYPE -1 4")
      READ(1.5) LAYER
      IF (IGRAF) 1709,35%
  C
C
          PRINTER DUTPUT
  17% #FITE(1:18%)
  162 FTREAT("TYPE IN S.DEPTH: START, STEP, END")
      RE= ) (1.4) 501.502.503
C
C
          OUTPUT MEADING ETC.
      CALL EXEC (3:11058:-1)
      IF (LAYER) 150,210
  199 %-ITE (5.228)
  200 FORMATICEX."THO LAYER MODEL"/)
      GO TO 230
  213 83175 (6,22%)
  227 FORTAT (20X - WHILT ILAYER HOUEL"/)
  23n aPITE (6,249)
  24/ FORMATON SUBJECT DEPTHMAXMEXTENSIONM7XMRANGEM6XMTHICKNESSM
          5X."5. VCLCCITY"/.4A,"METRES". OA, "METRES", 9X, "METRES".
     i
          6X. "METKES" . 1UX. "H/SEC")
C
          CALCULATE SOUNCE DEPTH ETC.
      NX=(503-501)/502+1.
      DO 344 1=1.4X
      SUE2=3' 1+FLUAT(I-1) #502
```

Vゥりゅからいちょうこん)

Vanaka EXHAX)

CALL FIVAL (0, V. SOMIN, VEL, IDEP, ITURN, 1) CALL, FIVAL (VOU. VEL OUEP. 19.N. 1TURN)

CALL MULTICORVEL . VCKIT . DCKIT . SDMIN . ICRIT . IDEP .

```
C
```

Õ

V.

```
CALCULATE SCALE FACTORS -
```

42% ISCSD=ISCAL (SDRAX) ISCT#=ISC#L(THEAK) ISCHA=ISCAL (RAHAR) ISCEX=ISCAL (EXHAX) DO 552 J=1.3

OUTPUT GRATICULE

CÁLL GRAT (ÍNA-JÉ) ÍSCSU - ĎCRIŤ - LÁYER - ISHAP) CALL DARK (528,644).

CALL ALPHA

IF (J-2) 432-462-492

438 #RÎTÊ (16.442) ÎSCÎH

449 FORMAT ("THICKNESS SCALE =", 15," H/UNITH)

CALL DARK (912, 15) CALL ALPHA

WRITE (15,45%)

450 F024AT ("TrīCKVĒSŠ+")

GC TO 524

453 ##ITE(16,470) ISCRA

476 FORMAT("RANGE SCALE =", IS, MA/UNITA)

CALL 948K (\$12,15)

CALL ALPHA

WRITE (15,489)

439 FURHAT ("RANGE+")

60 TO 520

493 WRITE (16.52%) ISCEX

500 FORMAT ("EATENSION SCALE =",15," M/UNITH)

CALL DEKK (912,15)

CALL ALPHA

WRITE (16,518)

510 FORMAT ("EXTENSION+")

529 STEP=(SDHAX-DD)/186.

C C C

OUTPUT RESULTS

DC 553 I=1.133 SDEP=D%+FLOAT(I) #STEP

IF (J-2) 525.539

525 IF (LAYER) 538,540

53% CALL THO (V% - VCKIT - DCRIT - SDEP - DM - DTURN - VTURN -1

RA(I) •EX(I) •Tm)

60 TO 588

540 IF (SDEF-DTURN) 552,568

55% CALL FIVAL (0, V. SOEP. VEL, IDEP. ITURN. 1) CALL FIVAL (V.D. VEL, DEP. 19.4. ITURN)

GO TO 570

560 CALL FIVAL (D. V. SDEP . VEL . IDEP . N. ITURN)

CALL FIVAL (Y,D, VEL -DEP, 19, 10, ITURN)

CALL FIVAL (D. V. DEP. VEL. 17. ITURN. 1)

CALL FIVAL (V.D. VEL. DEP, 18, 17. ITURN)

57% CALL MULTI(VØ.VEL, VCRIT.DCHIT.SDEP, ICRIT. IDEP, V.D.

THE PARTICULAR PROPERTY OF THE PARTICULAR PROPERTY OF THE PARTICU

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保承(1)。但以(1))
      THEDED
C
C
          CALCULATE CO-UNDINATES FOR DISPLAY
  584 IF (J-2)598.584.619
  594 Ix=(TA/FLU4T([SUT=1)=254.+23.
     60 TO 629
  5#& [x=(4A(1)/FLO3[(15C/A))#2ve.+23.
     GG TO SES
  613 IX=(Ex(I)/FLU4T(ISCEX))=252.+23.
  62@ IY=531.-(50%P/FLOAT(ISCSD))@12%.
      IF (I-2)63&+>44
  639 Call Dank (IX. II)
      GG TO 558
  64% CALL BRIGHTIA-IY)
  654 CG4TINE
      CALL HERDC
  552 CONTINUE
     CALL DAKK (3e+331)
      CALL ALPHA
C
          RECUEST IF EXPANSION IS REQUIRED
      #FITE (16.574)
  67a FORMAT ("TÜ EKPAMI PLUT PUSITION CURSOR AT MAXIMUM SOURCE "•
           "GEPTH REGULACO AND TYPE 1"./.34X,"OTHERRISE TYPE O")
      CALL CURSI (ICHAR, [A-1Y)
      IF (IC-12-14-49) 710+630
C
C
          CALCULATE HEW HAXIMUM SOURCE DEPTH
  69# S0%4X=(631.-FLOAT(LY))/120.%FLOAT(ISCSD)
      IF (5044A-UCKLI*6.95) 198,698
  698 SUMAX=OCKIT=0.95
  706 GU TO 366
  718 CALL EMASE
      CALL HUME
      60 10 1500
 C
C
          CALCULATION AND DISPLAY OF SHAUDY ZONE SHAPE
  729 HRITE(1-189)
      READ(1.4)501.502.503
      IF (5:11-0100 1-1.) 730. 74%
  730 SD1=DTURN+1.
  740 IF (502) 752 • 750 • 160
  75: 514=1
      60 TU 785
  75" IF (SD3-5U1) /7%,77%,780
  770 41 = 1
      Gú Tu 705
  780 81x=(503-501)/562+1.
C
```

```
C
          FIRD MAKIMUM VALUES
  785 SEEP=501
      CALL FIVAL (U-V, SUEP) VSDEP, ISDPT, N, ITUNN)
      CALL FIVAL (Y-D-VSDEP-DMAX-1-10-ITURA)
      CALL FIVAL (8-4-93AA-VI-11-1TURNOI)
      CALL FIVAL (V.D.VI.UMAX, I. II. ITURN)
      DG 79% I=2.3
  799 C(I)=(b(I)-0(I-1))*(v(I)+v(I+1))
      Z=()444-04)/128.
      CALL DETES (2+DE+SUEF+VSUEP+ISDPT+UMAX+I9+ITURH+N+
          C-O-V-UIST1-UIST2-RAU)
C.
C
          CALCULATE SCALE FACTORS
C
      ISCTH=ISCAL (DHAX)
      ISCRA=ISCAL(DIST2)
C
          OUTPUT GRATICULE
      CALL SHAT (HAME, ISCTH, DCRIT, LAYER, ISHAP)
      CALL DARK (688-544)
      CALL ALPHA
      WRITE (16,472) ISCRA
      CALL DARK (2.2)
      CALL ALPHA
      IF (¾X-2) 698+918
  89% MRITE(15.799) S01
  988 FOR 4AT ("SOURCE DEPTH =""F6.1" METERS +")
      60 TO 934
  912 #RITE(16,920) S01, S03, SD2
  928 FORMAT ("SUURCE DEPTH =",F6.1," M TO",F6.1,
          " # IN STEPS OF" F6.1," ME")
     1
  930 CALL DARK (912:15)
      CALL ALPHA
      WAITE (16,489)
      DO 1132 J=1.NX
C
C
           CALCULATE RESULTS
      SDE?=SDI+FLOAT(J-1) 4SD2
      CALL FIVAL (D. V.SDEP, VSDEP, ISDPT, N. ITURN)
      CALL FIVAL (V.D. VSULP. DMAX. II. 10. ITURN)
      CALL FIVAL (3. V. DMAX. VI. II. ITURN. I)
      CALL FIVAL (V+0+V1+DM4X+I2+I1+ITUKN)
       STEP=(DMAX-00)/100.
       Z0L01=9.
       ZGLJZ=-1.
      RNE#1= /.
      RNE *2=1.E13
      RADI=#.
      RAD2=%.
      DO 1050 1=1+100
       Z=FLOAT (I) #STEP
       CALL DETPS (Z+DU+SDEP+VSDEP+ISDPT+UMAX+IN+ITURN+N+
           C+D+V+DISTI+DISTZ+RAD)
      1
```

```
FIND WHICH POINTS TO RETAIN
      ÎF (BADI) 942.940,950
 948 23:432=3:4261 ...
      60 TO 562
  95% E=(Z-ZELU1)/2AU1
     RANGE===E+1+7401750RT (E# (2.-E))
  954 IF (DISTI-#4%)E) +7%+980
  974 Ra(I)=RANGE
      GO TO 490
  989 882-1=91571
      RA(I)=01571
      ŽÓLÐ1≐Ž
      RADITERAD
  996 IF (RADZ) 1666-1819
 1939 RANGE=ENENZ
      GC TO 1424
 1312 E=(Z-ZOLO2)/RAD2
      RANGE==MEH2-9402#5u+T(E#(2.-E))
 1022 IF (RANGE-UIST2) 1030, 1040
 1939 Ex(1)=24NGE
      GO TO 125%
 1946 R 4E 52=0IS12
      EX(I)=@IST2
      ZOLD2=&
      RAD2=RAD
 1050 CONTINUE
C
          DISPLAY RESULTS
      DO 125. I=1,100
      Z=FLOAT(I)#STEP
      IA=(R4(I)/FLOAT(ISCHA))#200.+23.
      IY=531.-(Z/FLOAT(ISCTH))#12%.
      IF (1-2) 126%, 1070
 1668 CALL DARK (IX+IY)
      GO TO 1380
 1070 CALL BRIGH(IX+IY)
 1030 CONFINCE
      DO 109/ 11=1.100
      I=131-11
      Z=FLOAT(I)#STEP
      IX=(EX(I)/FLOAT(ISCRA))#202.+23.
      IY=531.-(Z/FLOAT(ISCTH))#120.
 1090 CALL BriGa(IX.IY)
 1100 CONTINUE
      CALL HARDO
      CALL EMASE
      CALL ALPHA
      CALL HOME
      GO TO 1500
  C
          REQUEST NEXT OPERATION
```

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PAGE Madis
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```
PAGE 9241
 FTNOL
 C
            J.P. 22-11-71
 C
 C
            THIS IS THE FIRST SET OF SUBROUTINES FOR THE
 C
        PROGRAW SHAZO
 C
       SUBROUTINE MULTI(VØ. VEL. VCKIT. DCRIT. SDEP. ICRIT. IDEP.
            ValaKANGE , EXT)
       DIME ISION V(1).J(1),T(40)
 C
 C
            THIS SUPROJEINE CALCULATES THE RANGE AND EXTENSION OF
 C
       THE SHIDDS ZONE FOR THE MULTILAYER MODEL.
 C
       DCRI=0(ICaIT)
       (TIFJI) V=1hOV
       DO 19 I=> ICHIL
    10 T(I)=SakT((V0+V(I-1))*(V0-V(I-1)))+SQRT((V0+V(I))*(V0-V(I)))
       DEP1=)(IUEP)
       VELI=V(IDEP)
                                        Reproduced from best available copy.
C
           CALCULATE EXTENSION
       IF (DEP1-UCP1) 20,30
    2% I=IDEP+1
       DEP2=0(1)
       VEL2=v(1)
       S=SJRT((V0+VEL)*(V0-VEL))+SQRT((V0+VEL2)*(V0-VEL2))
      EXT= (DEP2-SUEP) * (VEL+VEL2)/S
      S=SQRT((V&+VCRI)*(VA-VCRI))
      EXT=EXT+(UCHIT-DCHI)*(VCRIT+VCRI)/S
       GU TO 40
   30 EXT=(DCPIT-SUEP)*(VCHIT+VEL)/SORT((VO+VEL)*(Vd-VEL))
   40 IF (DEP2-UCH1)50.70
   50 I1= IDEP+2
      DO 50 [=II.ICAIT
   60 EXT=EXT+(0(1)-0(1-1))*(v(1)+v(1-1))/T(1)
   70 EXT=EXT#2.
C
C
           CALCULATE RANGE
C
      S=SQRT((V0+VEL1)*(V0-VEL1))+SQRT((V0+VEL)*(V0-VEL))
      RA 15== (SUCH-UEPI) * (VEL+VEL1) /S
      00 50 1=2, IUEP
   80 RANGE=-20NA-(([-1))/(([-1))/+30NA-=30NAR
      RETUR.
      END
C
C
```

```
SUSROUTINE TWO (VW. VC-IT-DCRIT, SDEP-DØ, DTURN,
          VTURNOPANGE OF A TOTALCKE
C
C
          THIS SUBROUTINE CALCULATES THE RANGE, EXTENSION AND
C
      THICKNESS OF THE SHAUOW ZONE FOR THE 2 LAYER MODEL.
      IF (OTJen-Suich) 10.20
   10 VEL=VTURN+ (VCRIT-VIURN) & (SUEP-DTURN) / (DCRIT-DTURN)
      S=SQRT((V0+VEL) # (V0-VEL))
      EXT=2.* (DCFIT-SDEP) * (VCRIT+VEL) /S
      S=S+SPFT((V&+VTURA)*(VØ-VTURN))
      PANGE=(SDEP-DTURN) * (VTURN+VEL) /S
      RANGE=FANGE+DTURN*(Vv+VTURN)/SQRT((VØ+VTURN)*(VØ+VTURN))
      THICK=D8+(DTURN-D0)*(V0-VEL)/(V8-VTURN)
      GC TO 38
   20 VEL = VTJRN+ (VU-V [UKN) # (SDEP-DTURN) / (DU-DTURN)
      S=SJRT((V&+VTUKN)*(VN-VTURN))
      RANGE=SDEP*(VØ+VEL)/S
      EXT=2. # (UCRIT-DTURN) # (VCRIT+VTURN) /S
      S=S+SQ2T((V0+VEL)*(VU-VEL))
      EXT=EXT-2.# (SDEP-UTURN) # (VEL+VTURN)/S
      THICK=DTURN+(DCKIT-DTURN)*(VEL-VTURN)/(VØ-VTURN)
   30 RETURN
      END
                     Reproduced from sailable copy.
C
C
PAGE JUU3
      SUBROUTINE BIRAN (V.D.N.S.PHI)
      DIMENSION V(1) .D(1)
C
C
           THIS SUBROUTINE CALCULATES THE SOUND VELOCITIES V(I)
C
      AT DEPTHS D(I) FROM THE TEMPERATURE VALUES INITIALLY
C
      STORED IN ARRAY V. S IS THE SALINITY AND PHI THE
C
      LO 1301 TUUÉ
      DO 10 I =1 + iv
      V(I) = 1.493.+3.*(V(I) - 10.) - 0.006*(V(I) - 10.) *(V(I) - 10.)
          -2.34*(v(1)-18.)*(v(1)-18.)+1.2*(S-35.)-0.01*
     1
           (V(I)-18.)*(5-35.)+D(I)/61.+1.E-7*D(I)*D(I)
     2
           +2.E-1/*U(1)*U(1)*(V(1)-18.)*(V(1)-18.)+1.E-4*
          Q(I) *~HI/Au.+2.oE-4*V(I)*(V(I)-5.)*(V(I)-25.)
   10 CONTINE
      RETURN
      END
C
C
```

```
SUBROUTINE FINTP(V+V+ITUKN)
      DIMENSION V(1)
C
          THIS SUBROUTINE FINDS THE MINIMUM ELEMENT OF
CC
      APRAY V AND PLACES ITS SUFFIX IN LOCATION ITURN
      VMIV=V(1)
      N.S=1 NS 00
      IF (V(I) - v#I4) 13,20
   10 V~IN=V(I)
      I=VivI
   20 CONTINUE
      ITURV=[4]N
      RETURN
      END
C
C
PAGE 0005
      SUBROUTINE FIVAL (A.B. VALUE, RESLT, ISSCK, NI, N2)
      DIMENSION A(1), B(1)
C
C
          THIS SUBROUTINE FINDS THE VALUE IN ARRAY B WHICH
CCC
      CORRESPONDES TO "VALUE" IN ARRAY A AND PLACES IT IN
      RESLT. NI AND NZ ARE THE LIMITS OF THE ARRAY SUBSCRIPTS
      SO ARRANGED THAT NO IS THE SUBSCRIPT OF THE LARGEST
Ċ
      VALUE OF A.
      N=IA3S(N1-N2)
      IF (N1-N2) 17,20
   10 INCR=1
      GO TO 30
   일상 INCR=-1
   30 00 50 Il=1+N
      I=N1+INCK*I1
      J=I-INCR
      IF (VALUE-A(I))50+40
   40 DEL=(VALUE-A(I)) '(A(J)-A(I))
      RESLT== (I) +DEL*(3(J)-3(I))
      ISSCR=I
      GO TO 60
   50 CONTINUE
   60 RETURN
      END
```

```
FINAL
C
          J. L. 27-13-/1
C
C
          THIS IS THE SECOND SET OF SUBHOUTINES FOR THE
C
      PRJ374. 5-120
C
      SUBPOUTTIVE GRAT (IMAME * ISCSO * DORIT * LAYER * ISHAP)
      DI E SIV 194 (1)
C
C
           THIS SUBROUTING PRODUCES THE BASIC GRATICULE FOR
C
      GRAPHIC DISPLAYS.
      CALL ETASE
      CALL HOME
      WRITE (15,1%)
   10 FORMAT(/)
      CALL DINUBL
      IF (ISmar) + 0.21
   2/ WPITE(16+3/)
   30 FOR 14T (2(x . "+")
   40 WEITE (16.50) (INAME (I). I=1.6)
   50 FORMAT(12x+"X & T "+6(X+A1)+"+")
      IF (LAYER) 50,80,100
   60 WRITE (15,70)
   70 FORMAT (22x+4T & 0
                            LAYER")
      GO TO 124
   80 WRITE (15+9/)
   90 FOR 44T(X)
      GU TU 120
  100 WAITE (16.110)
  110 FURMAT(22X+"M U L T I L A Y E R")
  120 CALL ALPHA
      WYITE(16,130) JCRIT
  130 FORMAT(/,27x,"CRITICAL DEPTH =".Fd.2," METRES")
      IF (IS-18)148,160
  140 WRITE (16.150)
  15% FORMAT (6X+"SOURCE +")
      GO TO 180
  160 WPITE (15,170)
  170 FORMAT(13x,"+")
  187 92 [TE &16 . 19 ) [SCSU
  190 FORMAT ("DEPTH SCALE = ", 15," M/UNIT")
      CALL DARK (23,031)
      CALL B-IG-(23.31)
      CALL Baller (1023,31)
      CALL BRIGH (1023+631)
       CALL 9-16m(23.631)
      DO 210 I=223.323.200
       CALL DARK (I+31)
       CALL 3716H (1.53)
       DO 222 J=63.533,16
  2NN CALL POINT(1,J)
       CALL DARK(I,597)
  210 CALL 5~167(1.531)
       Do 232 I=151,511,120
```

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: PAGE 3212
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1

```
CALL DARK (23.1)
      CALL 3-16m(55.1)
      00 22/ J=87.991.15
  224 CALL P.) [HT (J+1)
      CALL DAKK (991-1)
  234 CALL 5-IUH(1023.1)
      CALL DAKK (7+031)
      CALL ALPHA
      #RITE (16.24w)
  249 FORMAT ("#".//)
      IF (ISHAP) 250+270
  250 *PITE (15+25%)
  260 FOR 44T ("5"/"U"/"U"/"K"/"C"/"E"/)
  27# ##ITE(15,280)
  280 FORMAT ("D"/"E"/"P"/"F"/"F"/"H")
      RETURN
      END
C
C
PAGE
      ขะช3
      FUNCTION ISCAL (RAMAX)
      DIMENSIUM ISC(3) , XMAX(3)
C 1
          THIS FUNCTION TAKES THE NEXT VALUE ABOVE RAMAX FROM
C
      THE SEVIES 141044N, 241044N, 541044N WHERE N=1.2.3....
Č
      ISC(1)=1
      ISC(2)=2
      ISC(3)=5
      XMAX(1)=5.
      XMAX(2)=10.
      XMAK(3)=20.
   10 00 30 I=1.3
      IF (XMAX(I)-RAMAX) 30,20
   24 ISCAL=ISC(I)
      GO TO 50
   30 CONTINUE
      DO 40 I=1.3
      ISC(I)=1&*ISC(I)
   40 XMAX(I)=10.4XMAX(I)
      GO TO 10
   50 RETURN
      END
C
```

```
Surp If the Datable Suep, asdep, isdatodax, id, itura, n,
         Colovouistionisteorau)
      01 * Ension C(1) * 0(1) * v(1)
C
          THIS SUBHOUTINE CALCULATES THE DISTANCES TO THE
C
      VOLTERS OF HAYS BRICH VORTEX AT A DEPTH Z AND ALSO
C
      THE RACIUS OF THE WAYN AT THESE POINTS
C
      PS:(4+1)=50x[((4+1)*(4-6))
C
C
          FI'D VELUCITY AT DEPTH Z ETC.
C
      DS ) ? [ = 0 ( 150 P T )
      V502T=4(I504T)
      CALL FIVAL (U+V+Z+SK+1ZPT+1TUK4+10)
      IZ=T=17FT+1
      DZ21=0(122T)
      VZPT=V(IZPT)
C
          SK=SMELLS CONSTANT FOR THE RAY
C
      CALL FI ME ( /+ ) + ST + OLZ + ILZPT + N+ ITURN)
      ULZPT=0(1LZPT)
      VLZ^2T=y(ILZ^2T)
C
C
          FIND THE DISTANCE TO THE FIRST TURNING POINT
C
      DISTI='.
      IF (1.E-4-18LE2+18271)3,7
    3 DISTI=(SUEF-USDPT) * (VSDEP+VSDPT)/(RSQ(SK. VSDPT)+RSQ(SK. VSDEP))
    7 IF (ISDPT-12PT) 10,30,10
   1 1 2=1737-1
      14051 FC=1 F2 CG
      IF (SK-V([-1))17+13
   13 IF (SK-/(I))17,20
   17 DISTI= .
      DIST2=1.Elv
      GO TO 140
   20 DISTI=DISTI+C(I)/(KSQ(SK,V(I-1))+KSQ(SK,V(I)))
   30 IF (1.E-4-5K+VZPT) 40,45
   45 DISTI=DISTI+(DZPT-Z)*(VZPT+SK,/RSQ(SK,VZPT)
C
C
          FIND THE DISTANCE TO THE SECOND TURNING POINT
   45 IF (Z=0MAX) 62.50
   IT21U=ST2IG NZ
      GO TO 140
   60 IF (JLZ-U(15U2[+1))76+70
   70 IF (1.E-4-5K+VSDEP) 80.140
   80 DIST2=UIST1+2.*(DLZ-SDEP)*(SK+VSDEP)/(RSQ(SK+VSDEP))
      GO TO 140
   90 DIST2=UIS(1+2.*(D(ISDPT+1)-SDEP)*(V(ISDPT+1)+VSDEP)/
          (RSQ(SK + V(ISDPT+1))+RSQ(SK + VSDEP))
      IF (ILZ-T-150PT-1)100.122.100
  100 J=150P1+2
      DO 112 I=J.ILZPT
```

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PAGE Ped5
```

```
11% DISTZ=01STZ+2.%C(1)/(RSQ(SK.V(1-1))+RSQ(SK.V(1)))-
12% IF(1.E-4-5*+VLZPT)13%.14%
13% DISTZ=01STZ+2.%(DLZ-DLZPT)*(SK+VLZPT)/RSQ(SK.VLZPT)
C
C CALCULATE RADIUS AT TURNING POINTS
C
14% RAD=5<%(DZPT-D(1ZPT-1))/(V(1ZPT-1)-VZPT)
RETURN
END
```